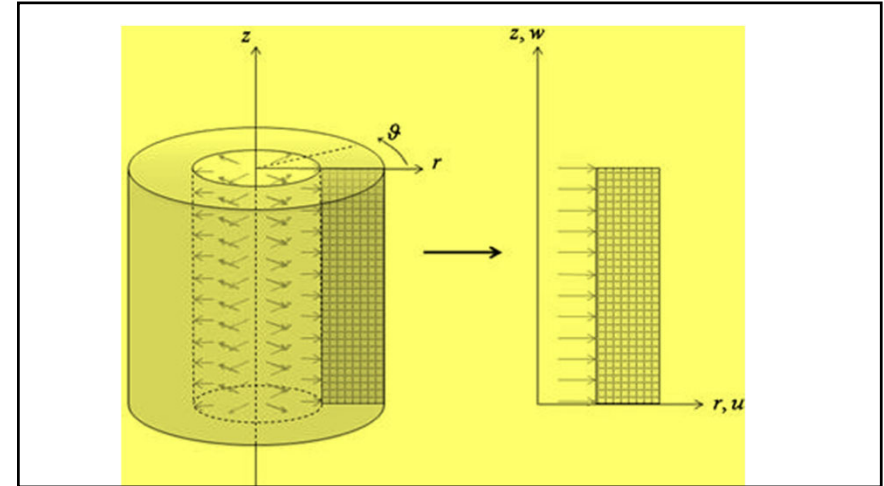


3.4. Two-dimensional element for the study of axisymmetric problems:

The symmetry is considered around the z-axis:

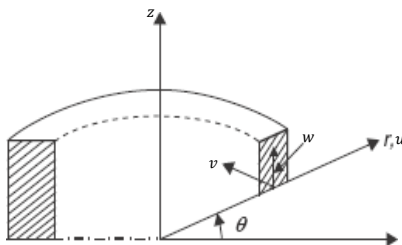
Due to this symmetry, every vertical section in the cylinder undergoes the same stresses and deformations, independently of θ ; therefore, the problem is reduced to a plane problem in the $r - z$ plane



Let's use the cylindrical coordinates r, θ, z related to the coordinates x, y and z by :

$$x = r \cos \theta, \quad y = r \sin \theta, \quad z = z$$

And denote the displacements in this reference system as: u, v et w



For the triangular element e will have:

3.4.1. Displacement field: $v = 0$

$$\begin{Bmatrix} u(r, z) \\ w(r, z) \end{Bmatrix} = \begin{bmatrix} N_1 & 0 & N_2 & 0 & N_3 & 0 \\ 0 & N_2 & 0 & N_2 & 0 & N_3 \end{bmatrix} \begin{Bmatrix} d_1 \\ d_2 \\ d_3 \\ d_4 \\ d_5 \\ d_6 \end{Bmatrix} \text{ where } \begin{Bmatrix} d_1 \\ d_2 \\ d_3 \\ d_4 \\ d_5 \\ d_6 \end{Bmatrix} = \begin{Bmatrix} u_1 \\ w_1 \\ u_2 \\ w_2 \\ u_3 \\ w_3 \end{Bmatrix}$$

With the same shape functions

$$N_1 = \frac{1}{2\Delta} [(r_2 z_3 - z_2 r_3) + r(z_2 - z_3) + z(r_3 - r_2)]$$

$$N_2 = \frac{1}{2\Delta} [(z_1 r_3 - r_1 z_3) + r(z_3 - z_1) + z(r_1 - r_3)]$$

$$N_3 = \frac{1}{2\Delta} [(r_1 z_2 - z_1 r_2) + r(z_1 - z_2) + z(r_2 - r_1)]$$

3.4.2. Deformation field:

The deformations are:

$$\varepsilon_r = \frac{\partial u}{\partial r}; \varepsilon_\theta = \frac{u}{r}; \varepsilon_z = \frac{\partial w}{\partial z}; \gamma_{r\theta} = \gamma_{\theta z} = 0; \gamma_{rz} = \frac{\partial u}{\partial z} + \frac{\partial w}{\partial r}$$

$$\varepsilon = \begin{pmatrix} \varepsilon_r \\ \varepsilon_z \\ \varepsilon_\theta \\ \gamma_{rz} \end{pmatrix} = \begin{bmatrix} \frac{\partial}{\partial r} & 0 \\ 0 & \frac{\partial}{\partial z} \\ \frac{1}{r} & 0 \\ \frac{\partial}{\partial z} & \frac{\partial}{\partial r} \end{bmatrix} \begin{Bmatrix} u \\ w \end{Bmatrix} = [B]\{d\}$$

$$\varepsilon = \begin{pmatrix} \varepsilon_r \\ \varepsilon_z \\ \varepsilon_\theta \\ \gamma_{rz} \end{pmatrix} = \frac{1}{2\Delta} \begin{bmatrix} z_2 - z_3 & 0 & z_3 - z_1 & 0 & z_1 - z_2 & 0 \\ 0 & r_3 - r_2 & 0 & r_1 - r_3 & 0 & r_2 - r_1 \\ \frac{N_1}{r} & 0 & \frac{N_2}{r} & 0 & \frac{N_3}{r} & 0 \\ r_3 - r_2 & z_2 - z_3 & r_1 - r_3 & z_3 - z_1 & r_2 - r_1 & z_1 - z_2 \end{bmatrix} \begin{Bmatrix} u_1 \\ w_1 \\ u_2 \\ w_2 \\ u_3 \\ w_3 \end{Bmatrix}$$

3.4.3 Stresses field:

$$\sigma = [C]\varepsilon$$

$$[C] = \frac{E}{(1+\nu)(1-2\nu)} \begin{bmatrix} 1-\nu & \nu & \nu & 0 \\ \nu & 1-\nu & \nu & 0 \\ \nu & \nu & 1-\nu & 0 \\ 0 & 0 & 0 & \frac{1-2\nu}{2} \end{bmatrix}$$

3.4.4 Stiffness matrix :

$$[k] = \int_V [B]^T [C] [B] \cdot dV = \int_0^{2\pi} d\theta \iint_{rz} [B]^T [C] [B] \cdot dr \cdot dz$$

$$[k] = 2\pi \iint_{rz} [B]^T [C] [B] \cdot r \cdot dr \cdot dz$$

There are two possibilities for evaluating this matrix:

The first is the explicit evaluation of the product $[B]^T [C] [B]$ and then the term-by-term integration;

The second is numerical integration. The simplest numerical integration procedure consists of evaluating all quantities for a centroid

$$\bar{r} = \frac{r_i + r_j + r_m}{3} \quad ; \quad \bar{z} = \frac{z_i + z_j + z_m}{3}$$

In this case::

$$[k] = 2\pi [\bar{B}]^T [C] [\bar{B}] \bar{r} \Delta$$

Where : $[\bar{B}]$ is the evaluation of $[B]$ at the element centroid point..