



Chapter 2.Static and total thermodynamic quantities in turbomachines

2-1-Types of thermodynamic transformations:

In turbomachines there are generally two types of transformations:

- a)-compressing
- b)-relaxing

These two types can be done in several ways:

Adiabatically, isentropically, isenthalpically, polytropically,.....

2-2-Visualization of a thermodynamic transformation:

1°)--for visualizations we generally use:

- a)-the entropy diagram (T-S)
- b)-the enthalpy diagram (h-S)

2°)--for the following interests:

-either for compression or relaxation, they directly visualize energy transfers

- a)-quantitatively on the ordinate: (example: for an ideal gas we have: $\Delta h = C_p \Delta T$)
- b)-qualitatively on the abscissa: (for an ideal gas we have: $\Delta S_{12} = C_p \ln \left(\frac{T_2}{T_1} \right) - r \ln \left(\frac{P_2}{P_1} \right)$)

2-3-Calculation of the parameters of a transformation:

1°)-isentropic transformation: ($dS=0$) of an ideal gas ($PV=RT$ et $\frac{C_p}{C_v} = \gamma$):

$$\text{if } \gamma = \text{const} \rightarrow \quad \text{a) } PV^\gamma = \text{const} \quad \text{b) } \frac{T}{P^{\frac{\gamma-1}{\gamma}}} = \text{const} \quad \text{c) } \frac{T}{V^{\gamma-1}} = \text{const}$$

2°) polytropic transformation (real):

the real evolutions 1-2 are often described by the equation of a polytrope:

$$P_1 V_1^k = P_2 V_2^k = P V^k = \text{const} \Rightarrow \frac{dP}{P} + k \frac{dV}{V} = 0, \text{ with } n: \text{ polytropic coefficient;}$$

$$\text{if } k = \text{const} \Rightarrow \quad \text{a) } \frac{P_1}{P_2} = \left(\frac{V_2}{V_1} \right)^k \quad \text{b) } \frac{T_1}{T_2} = \left(\frac{P_1}{P_2} \right)^{\frac{k-1}{k}} \quad \text{c) } \frac{T_1}{T_2} = \left(\frac{V_1}{V_2} \right)^{k-1}$$

Noticed :

► if we know the initial and final parameters of a transformation, we can calculate the polytropic

$$\text{coefficient } k: k = \frac{\ln P_1 - \ln P_2}{\ln V_1 - \ln V_2}$$

► The two types of transformations can be carried out in several ways depending on k: (Figure 2-0)

$k = \gamma$; isentropic compression or expansion (**reversible adiabatic**)

$k > \gamma$ (**theoretical case**); compression with heat input or cooled expansion

$k < \gamma$; cooled compression or expansion with heat input

$k = 1$; isothermal compression or expansion

2-4-Definition of an absolute stagnation variable:

► The stopping conditions are the conditions that would be obtained by a fictitious transformation bringing the fluid back to zero speed isentropically (reversibly and without heat exchange) and without exchange of useful work.

-For the enthalpy at point 2 includes the static enthalpy, the kinetic energy and the potential energy at 1 hence its name total enthalpy:

$$H = h_* = h_0 = h + \frac{c^2}{2} + gz$$

For an ideal gas: : $h_0 = C_p T_0$

- The total temperature: $T_0 = T + \frac{c^2}{2C_p} + \frac{gz}{C_p}$

- Total pressure: $P_0 = P + \rho \frac{c^2}{2} + \rho gz$

► Generally neglects the potential energy which gives:

-For the stagnation enthalpy: $H = h_* = h_0 = h + \frac{c^2}{2}$

-For an ideal gas: $h_0 = C_p T_0$

-For the stagnation temperature: : $T_0 = T + \frac{c^2}{2C_p}$

- Stagnation pressure and density: $P_0 = P + \rho \frac{c^2}{2}$

► For an isentropic transformation:

- Stagnation pressure and density: $P_0 = P \left(1 + \frac{c^2}{2C_p T}\right)^{\frac{\gamma}{\gamma-1}}$

- Stagnation density and $\rho_0 = \rho \left(1 + \frac{c^2}{2C_p T}\right)^{\frac{1}{\gamma-1}}$

► By introducing the Mach number: $M = \frac{c}{a} = \frac{c}{\sqrt{\gamma r T}} \Rightarrow \frac{c^2}{2C_p T} = \frac{\gamma-1}{2} M^2$

$$\Rightarrow T_0 = T \left[1 + \frac{\gamma-1}{2} M^2\right]; P_0 = P \left(1 + \frac{\gamma-1}{2} M^2\right)^{\frac{\gamma}{\gamma-1}}, \quad \rho_0 = \rho \left(1 + \frac{\gamma-1}{2} M^2\right)^{\frac{1}{\gamma-1}}$$

Or: $\frac{T_0}{T} = \left(\frac{P_0}{P}\right)^{\frac{\gamma-1}{\gamma}} = \left(\frac{\rho_0}{\rho}\right)^{\gamma-1} = 1 + \frac{\gamma-1}{2} M^2$ (**Generator state or Barré Saint V equation**)

- The fluid speed for adiabatic flow: $C = \left[\frac{2\gamma r}{\gamma-1} (T_0 - T)\right]^{1/2}$

- The flow reaches the maximum speed when $T=0$: $C_{max} = \left[\frac{2\gamma r T_0}{\gamma-1}\right]^{1/2}$

► **Critical state:** we speak of critical or sonic quantities when $M=1$:

$$\frac{T_0}{T^*} = \left(\frac{P_0}{P^*}\right)^{\frac{\gamma-1}{\gamma}} = \left(\frac{\rho_0}{\rho^*}\right)^{\gamma-1} = \frac{\gamma+1}{2} \quad \text{and the speed: } C^* = a = \sqrt{\gamma r T^*} = \left[\frac{2\gamma r T_0}{\gamma+1}\right]^{1/2}$$

- the case of entropy: $S = C_v \log \left(\frac{P}{\rho^\gamma}\right) = S_0$: It does not depend on the benchmark considered.

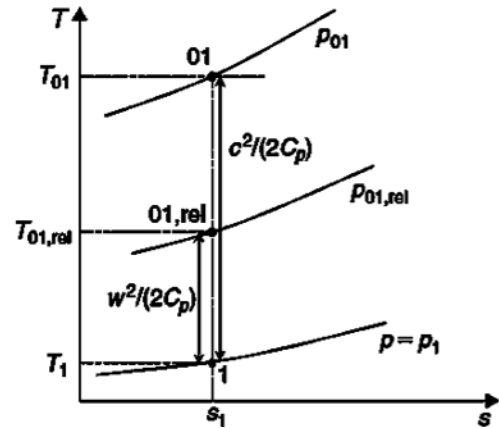


Fig.A : Relation entre la variable statique avec la variable d'arrêt absolue et relative sur un diagramme T-S

2-5-Definition of a relative stagnation variable:

- The relative stagnation enthalpy: $H_R = h_R = h + \frac{w^2}{2}$

-Relative stagnation temperature: $T_R = T + \frac{w^2}{2C_p}$

2-6-Calculation of static enthalpy gain and drop:

If $\gamma = \text{Cst}$, $R = \text{Cst}$, $k = \text{Cst}$, we can calculate either the gain or drop in enthalpy in the case of an isentropic or real transformation: (+: compression (gains), -: expansion (drop))

1°)-for an isentropic transformation:

$$\pm(h_{2s} - h_1) = \pm C_p(T_{2s} - T_1) = \pm RT_1 \frac{\gamma}{\gamma - 1} \left[\Pi^{\frac{\gamma-1}{\gamma}} - 1 \right]$$

2°)-for a real transformation: Real (effective) work:

$$\pm(h_2 - h_1) = \pm C_p(T_2 - T_1) = \pm C_p T_1 \left(\frac{T_2}{T_1} - 1 \right) = \pm RT_1 \frac{\gamma}{\gamma - 1} \left[\Pi^{\frac{\gamma-1}{\gamma}} - 1 \right]$$

With: $* C_p = R \frac{\gamma}{\gamma-1}$, $* \Pi = \Pi_C = \frac{P_2}{P_1} > 1$: compression rate $* \Pi = \Pi_D = \frac{P_2}{P_1} < 1$: expansion rate.

3°)-for a polytropic transformation:

The process can be described by the equation $PV^k = \text{Cst} \Rightarrow \frac{T_{2s}}{T_1} = \frac{T_2}{T_1} = \left(\frac{P_2}{P_1} \right)^{\frac{k-1}{k}}$

$$\int_1^2 (\pm dh) = \int_1^2 (\pm V dP) = \pm \frac{k}{k-1} \frac{P_1}{\rho_1} \left[\left(\frac{P_2}{P_1} \right)^{\frac{k-1}{k}} - 1 \right]$$

2-7-Calculation of absolute total enthalpy gain and drop:

1°)-for an isentropic transformation: With: $* C_p = R \frac{\gamma}{\gamma-1}$,

The process can be described by the equation $PV^\gamma = \text{Cst} \Rightarrow \frac{T_{02s}}{T_{01}} = \frac{T_{02}}{T_{01}} = \left(\frac{P_{02}}{P_{01}} \right)^{\frac{\gamma-1}{\gamma}}$

$$W_s = \pm(h_{02s} - h_{01}) = \pm C_p(T_{02s} - T_{01}) = \pm \frac{\gamma}{\gamma-1} \frac{P_{01}}{\rho_{01}} \left[\left(\frac{P_{02}}{P_{01}} \right)^{\frac{\gamma-1}{\gamma}} - 1 \right]$$

2°)-for a real transformation: Real (effective) work:

The process can be described by the equation $PV^k = \text{Cst} \Rightarrow \frac{T_{02s}}{T_{01}} = \frac{T_{02}}{T_{01}} = \left(\frac{P_{02}}{P_{01}} \right)^{\frac{k-1}{k}}$

$$W_r = \pm(h_{02} - h_{01}) = \pm C_p(T_{02} - T_{01}) = \pm \frac{\gamma}{\gamma-1} \frac{P_{01}}{\rho_{01}} \left[\left(\frac{P_{02}}{P_{01}} \right)^{\frac{k-1}{k}} - 1 \right]$$

3°)-for a polytropic transformation: $W_p = \sum(\pm dh_s) > \pm(h_{2s} - h_1)$

The process can be described by the equation $PV^k = \text{Cst} \Rightarrow \frac{T_{02s}}{T_{01}} = \frac{T_{02}}{T_{01}} = \left(\frac{P_{02}}{P_{01}} \right)^{\frac{k-1}{k}}$

$$W_p = \int_{01}^{02} (\pm dh_s) = \int_{01}^{02} (\pm V dP) = \pm \frac{k}{k-1} V_{01} P_{01} \left[\left(\frac{P_{02}}{P_{01}} \right)^{\frac{k-1}{k}} - 1 \right] = \pm \frac{k}{k-1} \frac{P_{01}}{\rho_{01}} \left[\left(\frac{P_{02}}{P_{01}} \right)^{\frac{k-1}{k}} - 1 \right]$$

Note1: for an isothermal transformation: (with: $\Delta h = 0$ and $\rho_0 = \frac{p_0}{rT}$)

The process can be described by the equation $PV = \text{Cst}$

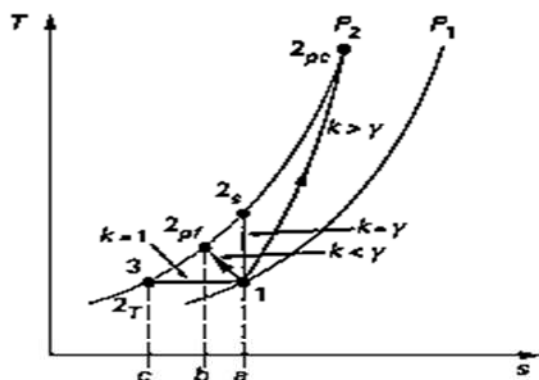
The work on the tree is: $W_{st} = -T\Delta S = rT \ln \left(\frac{P_{02}}{P_{01}} \right)$ or $\partial W_{st} = \frac{\partial p_t}{\rho_t} = rT \frac{\partial p_0}{p_0} \Rightarrow W_{st} = rT \ln \left(\frac{p_{02}}{p_{01}} \right)$

Note 2: - for compression the technical work: $W_{st} < (W_p)_k < \gamma < W_s < (W_p)_k > \gamma$

- for relaxation the work is in order: $|W_{st}| > |(W_p)_k < \gamma| > |W_s| > |(W_p)_k > \gamma|$

Thus, we will always seek to cool the gas during compression (never to heat it), we will often seek to heat a gas during expansion (never to cool it, except for possible questions of resistance of the materials to the temperature).

Canal comprimant



Canal détenant

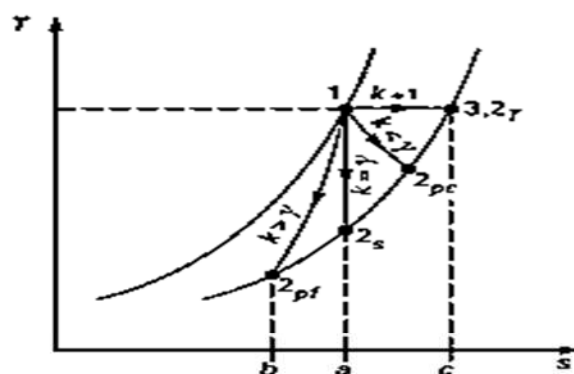
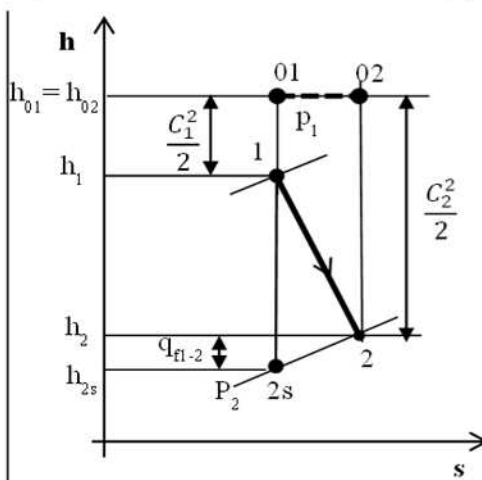
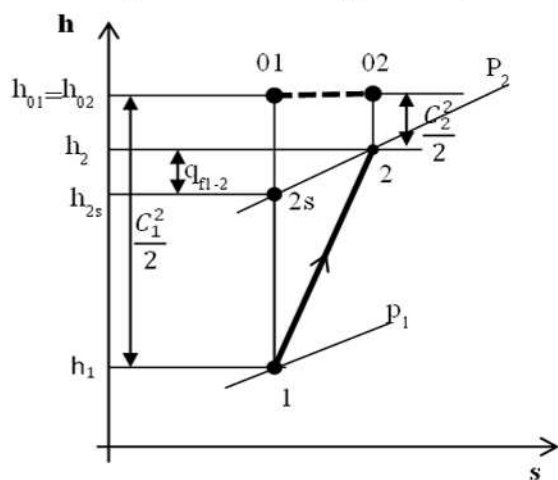
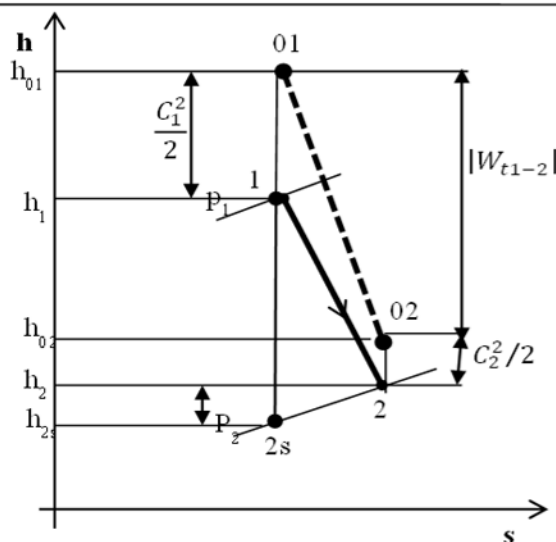
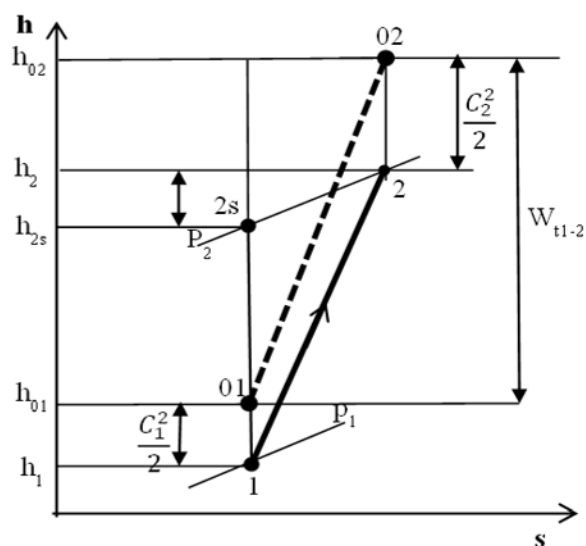


Fig-2-0- :- Visualizing isentropic and polytropic transformations on an entropy diagram (T-s)



Transformations finies

Fig-2-1- :-Transformation adiabatiques du fluide dans les canaux fixes



Transformations finies

Fig-2-2- :-Transformation adiabatiques du fluide dans les canaux mobiles

— Etat thermodynamique du gaz

----- Energie totale du gaz